



Research Article

# Impact of an Applied Magnetic Field on a High Impedance Dual Anode LANR Device

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## Abstract

This paper reports on the impact of an applied magnetic field intensity on LANR solution electrical resistance and an analysis of its role in metal deuteride loading and LANR performance. A dual anode PHUSOR<sup>®</sup>-type Pd/D<sub>2</sub>O/Au LANR device was driven at its optimal operating point, with two electrical current sources; to drive, and examine by 4-terminal electrical resistance, the loaded PdD<sub>x</sub> cathode. An applied magnetic field  $\sim 0.3$  T increases the LANR solution's electrical resistance  $\sim 10$ – $17\%$  with a time constant in minutes. The incremental resistance increase to an applied H-field is greatest at low loading current. The incremental resistance increase from an applied H-field is greatest with the applied H-field perpendicular to the driving electrical field (E-field) intensity. The modified LANR deuteron loading rate equation indicates that an applied magnetic field intensity increases deuteron loading in a LANR system by the increasing solution resistance and limiting undesired gas evolving reactions.

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*Keywords:* Deuterium, Deuterons, Excess heat, Excess power gain, Flux, Lattice assisted nuclear reactions, Loading, Metamaterials, Nanostructures, Optimal operating point, Palladium

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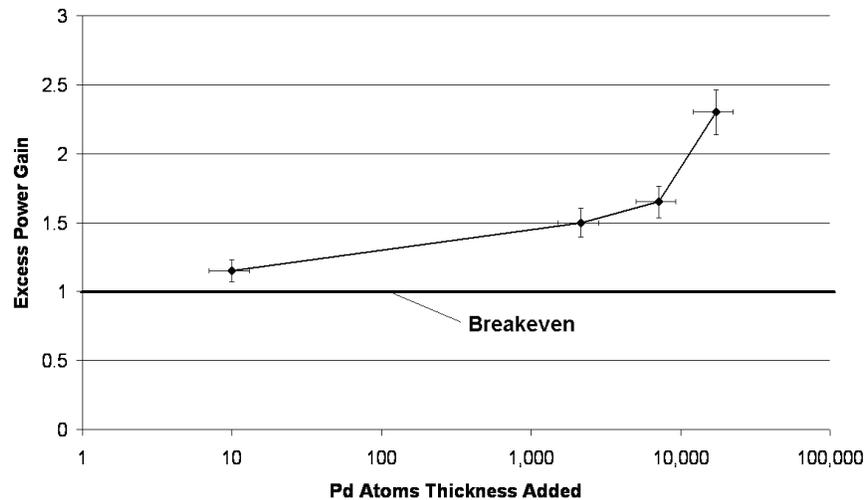
## 1. Lattice Assisted Nuclear Reactions

Lattice assisted nuclear reactions (LANR) use hydrogen-loaded alloys to enable near room temperature deuterium fusion and other nuclear reactions [1–49] using deuterons as fuel. Technologies which increase LANR excess energy production include thermal power spectroscopy [4], optimal operating point operation [1,3,4,24], the use of high electrical impedance solutions [3,4], metamaterial shapes [1,32] and nanostructures [1,37,60]. Correctly driven, LANR metamaterial nanostructured devices exhibit excess heat, excess heat flow, and non-thermal near infrared (NT-NIR) emission linked to both [34]. LANRs generated (“excess”) power densities range from  $\sim 7$  (1989 announcement) to  $80$ – $10,000$  W/cm<sup>3</sup>, today. Over time, the magnitude of generated excess power yields significant excess heat, and material changes which are wrought on the electrode, such as volcano-like pits [8,18,19].

At LANRs “core” are deuterons which are tightly packed into binary (“highly loaded”) metals and metallic nanostructures by an applied electric field or elevated gas pressure which supply deuterons in heavy water or gaseous deuterium.

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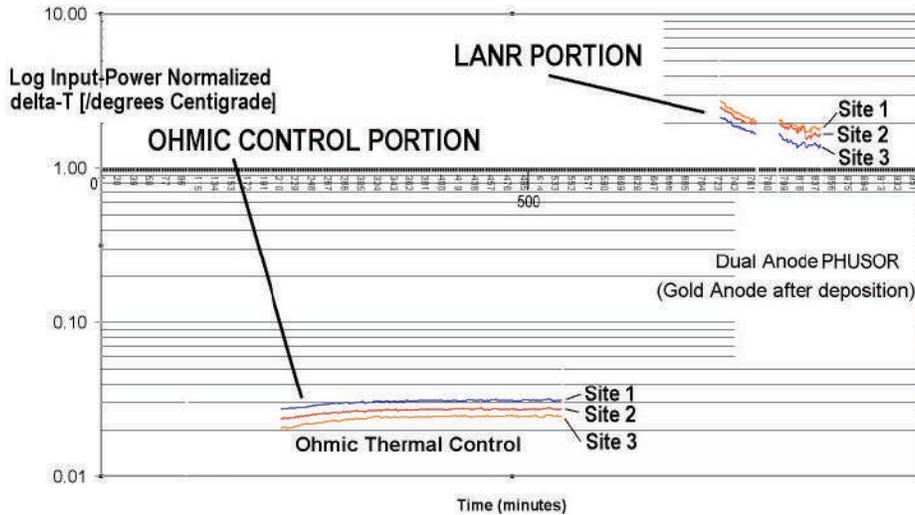


**Figure 1.** Excess Heat Correlated With Pd Codepositional Thickness Such high impedance metamaterial nanostructured LANR devices have shown power gains more than 200% and short term power gains to ~8000% [1,2], compared to input energy and to input energy transferred to conventional dissipative devices.

With control of LANR devices by precise nanostructure fabrication, metamaterial shape selection using high impedance (“High-Z”) PHUSOR<sup>®</sup>-type LANR devices in very high electrical resistivity (the real part of the complex impedance, with units of ohms) D<sub>2</sub>O, control of D-flux and post D-loading flux, there is a higher likelihood of achieving LANRs impressive energy gain, and with time integration – excess heat, with fairly good reproducibility.

Dual anode PHUSOR<sup>®</sup> LANR devices (DAP) use two anodes. The first is for preparation of the codepositional surface and solution, and the second is used to drive the active surface [37,68]. Investigations of DAP LANR devices (Fig. 1) have demonstrated that nanostructures are important in LANR with sizes involving circa 10 atoms or more in size. Corroboration of this fact includes experimental results in codeposition [25] and non-thermal near IR (NT NIR; Fig. 3) emissions [34]. The curve in Fig. 1 demonstrates with experimental evidence that LANR excess heat is correlated with the size of the Pd–D nanostructures, which can be considerable (Fig. 2). Figure 1 shows the monotonic increase in excess heat from LANR as the codepositional layer was increased in size over loaded palladium, apparently beginning with nanosize structures in temperature (degrees centigrade,  $\Delta T$ ) for both the ohmic thermal control and the DAP PHUSOR<sup>®</sup> type LANR device. The input power normalized  $\Delta T$  was used to compare the LANR and control (ohmic) systems over varying input powers. Sites 1 and 2 represent two sites within the active LANR cell. Site 3 was located at the ohmic (joule) control, consisting of a carbon resistor. In Fig. 2, over time, electrical power was first delivered to the control and then to the LANR device. The important point is that Fig. 2 demonstrates an LANR power gain of ~8000%.

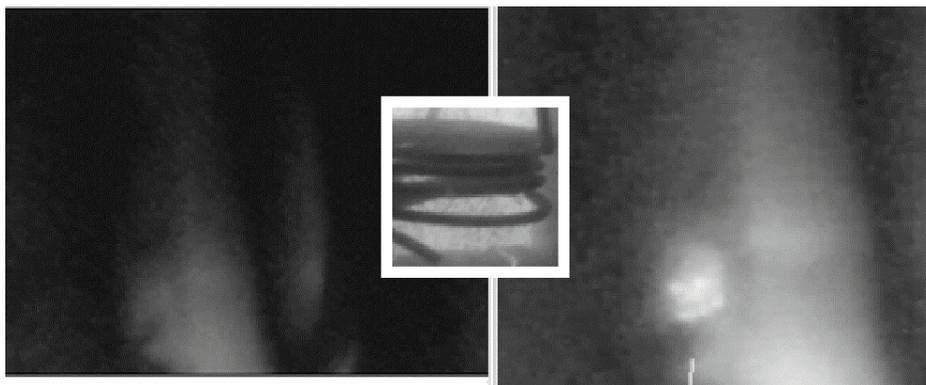
By imaging near infra-red, Fig. 3 shows a distribution of LANR activity over the surface of an LANR device, consistent with nanostructures. It shows the emission of near-IR from the electrodes when excess heat is only observed and the active electrodes operated at their optimal operating point (OOP; [1,2,57]), and then the nonthermal near IR emission (NT-NIR) is linked and specific to the LANR devices’ excess heat production and not its physical temperature [34]. This results from the temperature-related shift from hot fusion’s penetrating ionizing radiation to LANR’s skin-depth-locked infrared radiation [50]. Unlike hot fusion or plasma systems, bremsstrahlung radiant power density falls from 0.05 to 0.28 (hot fusion) to  $1.4\text{--}8.1 \times 10^{-10}$  for LANR. The delivered X-ray dose at 1 m decreases by incredible 18–



**Figure 2.** Input power normalized delta-T curves for DAP PHUSOR<sup>®</sup> LANR Fig. 2 shows the transient output of one DAP (Pd\*/D<sub>2</sub>O-Pd(OD)<sub>2</sub>/Au Dual Anode PHUSOR<sup>®</sup>-type) LANR device. The graph shows the input power-normalized change.

23 orders of magnitude from  $3.1 \times 10^{19}$  Grays (hot fusion) to  $\sim 2 \times 10^{-4}$  Grays for LANR. In addition, the temperature difference also causes the output spectrum of the Bremsstrahlung radiation to be shifted to the near infra-red, consistent with the NIR emission of LANR systems at their OOP. Figure 3 shows three visible and nearinfrared (NIR) views of a DAP codeposition PHUSOR<sup>®</sup>-type LANR device in heavy water. The platinum anode is seen in the background. The DAP PHUSOR<sup>®</sup> is located in both images ( $\sim 7.7$  mM Pd(OD)<sub>2</sub>). The inset view is in ordinary light, the other two (from a slightly different angle of observation) are in the near infrared (NIR). The image on the left precedes (“off”), and the one on the right is after activation and generation of excess heat of the PHUSOR<sup>®</sup>-type LANR system.

Given these LANR reactions, there has been much interest in the application of magnetic field intensities to LANR



**Figure 3.** Near-infrared images of DAP LANR cell, before and after activation, with close-up of cathode in visible light (inset) – after Swartz (2010; Ref. [34]).

systems. Dr. Pamela Mosier-Boss et al. at SPAWAR have reported morphology changes on the cathode with an applied magnetic field intensity [19]. For reasons that will become clear in the Interpretation section, because of the complex impact of laser irradiation of LANR cathodes upon solution electrical resistance and power gain [33], we elected to first report on the effect of those applied magnetic field intensities on LANR solution's electrical conductivity because that material parameter is decisive in the success of LANR systems.

## 2. Experimental Details

The six terminal LANR codepositional high impedance device used here was a DAP LANR device (Dual anode PHUSOR<sup>®</sup>-Type LANR device; Pd/D<sub>2</sub>O, Pd(OD)<sub>2</sub>/Pt–Au). It contains nanostructures whose preparation, assembly, and driving is complicated and described elsewhere [1,2, 3,4,34,35,37]. The LANR cathodes were prepared from 99.98+% Pd [Alfa Aesar, Ward Hill, MA], 1.0 mm diameter, ~ 4 – 7 turns on a spiral of ~1.3 cm diameter, with a gap separation from the anode arranged in a Pd/D<sub>2</sub>O/Pt or Pd/D<sub>2</sub>O/Au configuration (Pt 99.998%). The solution was 7.7 mM Pd(OD)<sub>2</sub> in low paramagnetic high electrical resistivity heavy water (deuterium oxide, low paramagnetic, 99.99%, Cambridge Isotope Laboratories, Andover MA) with no additional electrolyte. For the DAP devices, palladium is laid down from a sacrificial anode upon the surface of a palladium cathode. Then, the palladium anode is removed, and replaced by a gold wire anode to stop the further laying down of further palladium nanostructure upon the palladium cathode. Interestingly, we have reported a new phenomenon during codepositional layering of the DAP cathode. This consists of a dynamic instability oscillation, an electrohydrodynamic Rayleigh–Bernard instability associated with the layering. The time constant was circa 15 min per cycle, but this was irregular, with three to five cycles occurring in a 60 min period. Contamination remains a major problem, with excess heat devastatingly quenched by decreasing electrical resistance of the solution [2–4] the effects on the cathode can be minimized. Contaminants appear from both electrode and container degradation and leeching, from atmospheric contamination, and after temperature cycling. These all inexorably, unintentionally, add to the electrolytic solution decreasing the level of deuteron loading, the rate of loading as well, and the maximum heat producing activity. The heavy water is hygroscopic, therefore kept physically isolated from the air by seals, including several layers of Parafilm M (American National Can, Menasha, WI) and paraffin. All leads near the solution were covered with electrically insulating tubes (medical grade silicone, Teflon, or proprietary materials) used to electrically isolate wires. We continue to avoid chlorine or chloride because of possible explosions from visible light ignition susceptibility, which results because the activation energy with chlorine is only ~17 μJ.

The loading of the palladium from the heavy water, and driving of the reactions through the two electrodes within the reaction container was obtained by controlled electric current source, or a Keithley 225 at low input, with ±1% accuracy. Electrical voltage sources included HP/Harrison 6525A for transsample potentials up to 3000 V (~ ±0.5% accuracy). All connections isolated, when possible, with Keithley electrometers for computer isolation. To allow 4-terminal electrical resistance measurements within the loaded PdD<sub>x</sub> cathode, a first Keithley 225 electric current source was used to drive the cell, and load the cathode, and then a second Keithley 225 electric current source was used to drive the electrical current portion of the four terminal electrical resistivity measurement of the palladium. The data from voltage, current, temperatures at multiple sites of the solution, and outside of the cell, the 4-terminal measurement of the cathode's internal electrical conductivity, additional calibration thermometry and other measurements were sampled at 0.20 Hz, usually 1 Hz, 22+ bits resolution (Omega OMB-DaqTemp, voltage accuracy 0.015±0.005 V, temperature accuracy <0.6°C) and recorded by computed DAQ. To minimize quantization noise, 1 min moving averages were sometimes made. The noise power of the calorimeter is in the range of ~1–30 mW. The noise power of the Keithley current sources is ~10 nW. Input power is defined as  $VI$ . There is no thermo-neutral correction in denominator. Therefore, the observed power is a lower limit. The instantaneous power gain [power amplification factor (nondimensional)] is defined as  $P_{\text{out}}/P_{\text{in}}$ , as calibrated by at least one electrical joule control (ohmic resistor) and time integrated for validation. The excess energy, when present, is defined as  $(P_{\text{output}} - P_{\text{input}}) \times \text{time}$ .

The amount of output energy is interfered from the heat released producing a temperature rise, which is then compared to the input energy. Temperature measurements are made by specialized electrically insulated thermocouples [(accuracy  $\pm 0.8$  K, precision  $\pm 0.1$  K), RTD and other sensors. Probes were calibrated by Omega IcePoint Cell and core temperatures were maintained by feedback control using a Yellow Spring Thermal Controller Model 72 (bandwidth of 0.2 K) within a Honeywell water circulation zone controlled room ( $\pm 2.5$  K). Thermocouples and other temperature sensors decorated the periphery of the cell, and a multicompartiment calorimeter was used. There was an additional heat-flow probe at the periphery outside of the core. To minimize contamination, the majority of temperature measurements were outside of the inner core container. Calorimetry is augmented by heat flow measurement, electricity production using thermoelectrics, and LANR-driven motors. Outputs are calibrated by ohmic (thermal) controls, and dual ohmic (calorimeter) controls, to evaluate, and certify possible excess heat. Additional calibration has included adequate Nyquist sampling, time-integration, thermal ohmic controls, waveform reconstruction, noise measurement, and other techniques [2–4]. During the experiment, an attempt was made to determine, first, the impact of the direction of the electrical current used for the 4-terminal measurements along the cathode, and second, the impact of the direction of the applied magnetic field intensity obtained from neodymium magnets. The stationary applied magnetic field intensity was circa 0.3 T, and the field was directed either parallel or perpendicular to the applied electric field intensity used to load and drive the LANR device.

### 3. Results – Magnetic Fields

Within the DAP (Dual Anode PHUSOR<sup>®</sup>-type Pd/D<sub>2</sub>O/Au LANR) device, solution resistances ranged from 800,000  $\Omega$  initially to  $\sim 5000$   $\Omega$ . The 4-terminal cathodes measurements of electrical resistance of the loaded metal ranged from  $\sim 50$  to 120 m $\Omega$ . For the DAP device, the excess heat was measured as the thickness increased to  $\sim 17,000$  atoms deep (Fig. 1). At that time, the solution was 7.7 mM Pd(OD)<sub>2</sub>, and the open circuit voltage,  $V_{oc}$ , used to determine the effectivity of LANR [2,3], was 1.46 V. The Pd\*/D<sub>2</sub>O-Pd(OD)<sub>2</sub>/Au PHUSOR<sup>®</sup>-type system has an initial cell resistance of circa 868 k $\Omega$ , which fell to circa 48.3 k $\Omega$  upon final preparation.

For the DAP (Dual Anode PHUSOR<sup>®</sup>-type Pd/D<sub>2</sub>O/Au LANR device), applying a static magnetic field to the LANR system increased the solution's electrical resistance by 10–17%. This is shown in Fig. 4. The increase in solution electrical resistance was greatest at lower levels of electrical driving of the LANR system (1 mA vs. 10 mA). The increase in solution electrical resistance was greatest when the applied magnetic field was perpendicular to the driving electrical field intensity.

Figure 5 shows the time course of the changes to the magnetic field intensity. The time constant was on the order of minutes.

### 4. Interpretation – Deuteron Fluxes in LANR

An applied magnetic field in LANR can effect the resistance of the solution, and as will be shown below, that increased resistance can increase metal deuteride loading. Relevant to this analysis were our past studies which examined the impact of laser irradiation on LANR cathodes and reported, in 2003, that it decreases the solution electrical resistance and increases LANR excess heat, but decreases LANR power gain.

Deuteron flux is a key issue in LANR. Nernst calculations of the activities of the electrolyte [51,52] adjacent to a metal electrode have been applied to LANR to derive distributions of deuterium in palladium and the solution. However, because the LANR systems are not at equilibrium, such Nernst calculations are generally not applicable [53,54]. By contrast, unaffected by non-equilibrium, the quasi-1-dimensional (Q1D) model of deuteron loading [53] has been used to analyze deuteron populations and deuteron flow. It has foundation in the known dielectric properties of materials

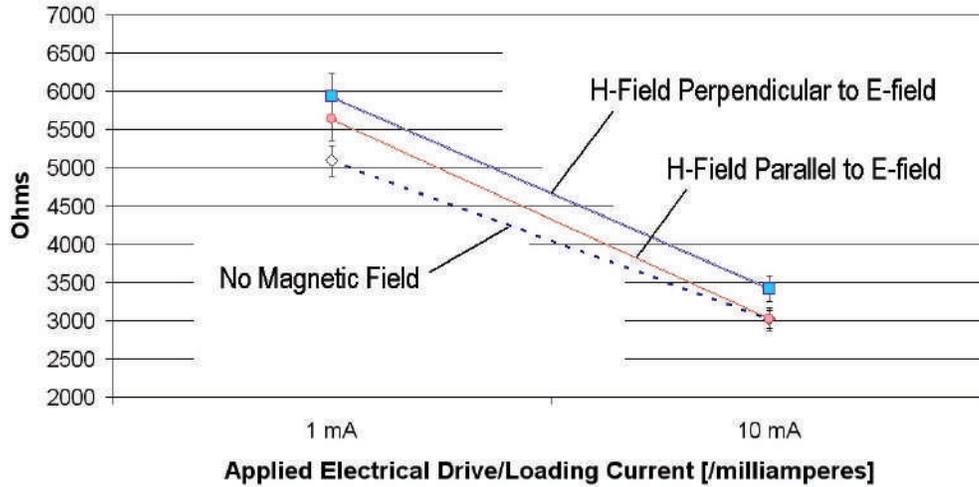


Figure 4. Effect of applied H-field on DAP PHUSOR®- LANR device’s solution electrical resistance.

[55] and continuum electromechanics [56], and has generated the deuteron-flux equations which explain the reason for LANR’s difficulty – and the road to success.

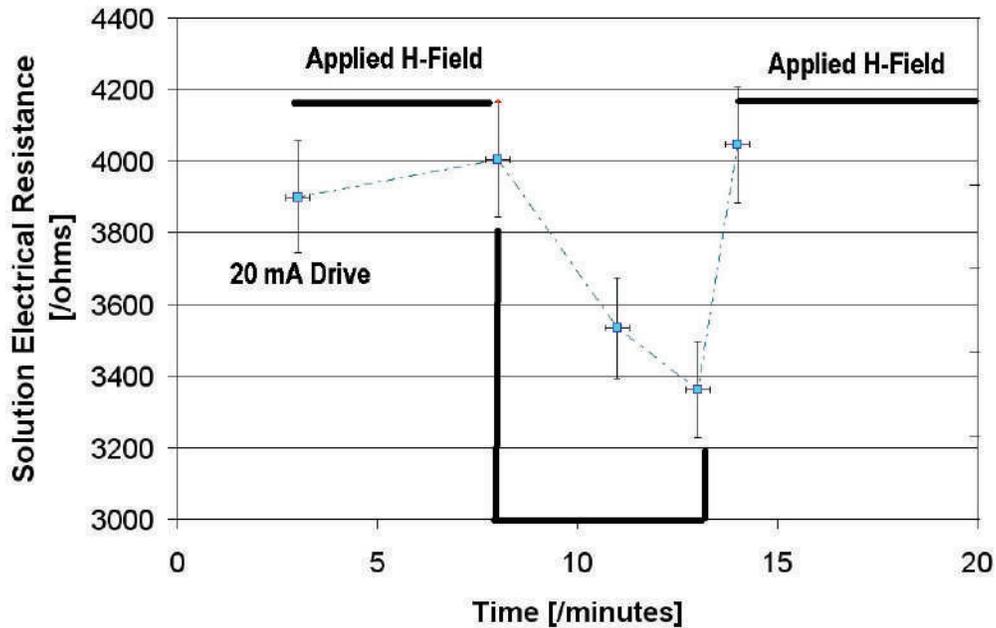


Figure 5. Time course of solution electrical resistance after change of applied H-field.

Several different deuteron populations and fluxes must be distinguished [57] at the surface of the low hydrogen-overvoltage palladium, with its surface highly populated with atomic, diatomic ( $D_2$ ), and bulk-entering deuterons [1,32]. The deuteron fluxes are seen on the left of Fig. 6, which is a schematic, simplified, representation of the anode, solution, and a portion of the cathode along with five types of deuteron fluxes involved in LANR.

The deuteron fluxes are deuteron cationic flow in the solution ( $J_D$ ), and the four types of deuteron flux in the loaded palladium cathodic lattice ( $J_E$ ,  $J_G$ ,  $J_F$ , and  $J_{IP}$ ). The latter are the entry of deuterons to the metal lattice (“loading”,  $J_E$ ), movement to gas ( $D_2$ ) evolution (“bubble formation”,  $J_G$ ), intrapalladium deuteron flux ( $J_{IP}$ ) flow through the metal (generated by metamaterials), and an extremely tiny loss by the desired fusion reactions ( $J_F$ ). There is conservation of deuterons with the exception of a loss ( $J_F$ ) to all putative fusion reactions, which are extremely small, when present.

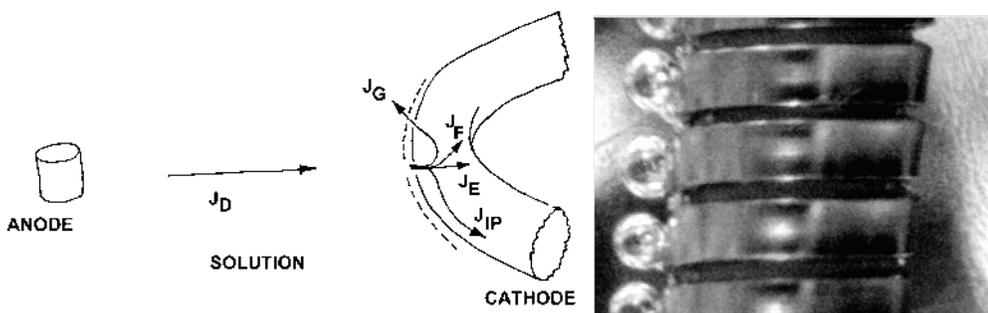
As Fig.6 shows, cationic deuteron flux ( $J_D$ ) brings deuterons to the cathode surface to create a cathodic fall and double layer before the electrode surface. It begins far from the cathode surface, in the deuterium oxide (heavy water) located between the electrodes, where the deuterons are tightly bound to oxygen atoms as  $D_2O$ . In the absence of significant solution convection, the flux of deuterons ( $J_D$ ) results from diffusion down concentration gradients and electrophoretic drift by the applied electric field [53,54,56,58].

$$J_D = -B_D \frac{d[D(z, t)]}{dz} - \mu_D [D(z, t)] \frac{d\Phi}{dz}, \quad (1)$$

$J_D$  depends on deuteron diffusivity ( $B_D$ ) and electrophoretic mobility ( $D$ ), and the applied electric field intensity. At any molecular site across the heavy water solution, the applied electrical energy is a tiny fraction compared to  $k_B T$ , so the deuterons migrate by drift ellipsoids of L- and D-deuteron defects in the applied electric field creating a ferroelectric inscription [58,59]. This D-defect conduction/polarization process augments other charge carriers, ionic drift, space charge polarization and clathrates. The resultant D-defect migration produces a “cathodic fall” of deuterons and a E-field contraction so that most of the voltage drop is at the interface in front of the electrode surface. This concentration polarization may produce very large local electric field intensities, possibly ranging from  $10^4$  to  $10^7$  V/cm [53,54].

From the concentration polarization of deuterons before the cathode, at the inner boundary of the double layer, intermolecular deuteron transfer from the heavy water solution to the metal surface is controlled and limited by electron-limited transfer, which leaves an atomic deuteron on the metal surface. The transfer mechanisms to the palladium surface are driven by infrared vibrations and microwave rotations [33,59], creating a solution photosensitivity which produces a photo-activated increase of excess energy and loss of power gain [33].

On the metal surface, the plethora of atomic deuterons either enter the metal (“are loaded”) forming a binary alloy [60–67], or remain on the surface, or form diatomic deuterium gas bubbles ( $D_2$ ). As a result, palladium has its



**Figure 6.** Deuteron Fluxes in LANR (a) Left – Schematic of deuteron fluxes, from solution to loaded metal. (b) Right – Close-up of active LANR cathode (after Swartz 2006, Ref. [17]).

surface populated with atomic (D) and diatomic deuterium ( $D_2$ ). Any deuterons which enter the metal are electrically neutralized ('dressed') by a partial electronic cloud, shielding their charge (in a Born–Oppenheimer approximation) [37]. The deuterons drift along dislocations and through the lattice and its vacancies, falling from shallow to deeper located binding sites. There is competing obstruction by ordinary hydrogen and other materials at interfaces and grain boundary dislocations. The gas bubbles ( $D_2$ ) are undesirable producing low dielectric constant layers in front of the electrode, obstructing the electrical circuit. As derived elsewhere [53], after solving the partial differential equations, and using conservation of mass, and numerically dividing each deuteron flux ( $J_E$ ,  $J_G$ , and  $J_F$ ) by the local deuteron concentration to yield the first-order deuteron flow rates,  $k_E$ ,  $k_G$ , and  $k_F$  (with units of cm/s, respectively), Eq. (2) is the deuteron flux equation of LANR. Numerically,  $k_e$  might be in the range of 0.5–30  $\mu A$ , and the concentration of (D) is circa 50 M.

$$k_e = \mu_D E - (k_g + k_f). \quad (2)$$

Equation (2) is the deuteron loading rate equation. It relates cathodic deuteron gain from the applied electric field to the loss of deuterons from gas evolution and fusion, and teaches many things. The deuteron loading rate equation shows that the deuteron gain of the lattice [through the first order loading flux rate ( $k_E$ )] is dependent upon the applied electric field *minus* the flux rate losses of deuterons from gas evolution ( $k_G$ ) and fusion ( $k_F$ ). The deuteron loading rate equation, Eq. (2), reveals that desired LANR reactions are quenched by electrolysis, which is opposite conventional "wisdom" that LANR is 'fusion by electrolysis'. Equation (2) also heralds that LANR can be missed by insufficient loading, contamination (effecting  $k_E$ , by protons or salt) and by the evolution of  $D_2$  gas, which all inhibit the desired LANR reactions [53,1,2] and leading to the optimal operating point manifolds. This quenching is of prime importance.

Equation (2) can be modified to Eq. (3), the modified deuteron loading rate equation, by substituting into it the Einstein relation. There are many important lessons for LANR.

$$k_e = \frac{B_D q V}{L [k_B T]} - (k_g + k_f). \quad (3)$$

The first term now has geometric and material factors.  $B_D$  is the diffusivity of the deuteron.  $k_B T$  is the Boltzmann's constant and temperature.  $q$  is the electronic charge, and  $V$  is the driving applied voltage. Most importantly, dominating the first term is the ratio of two energies (the applied electric energy organizing the deuterons divided by  $k_B T$ , thermal disorder). This energy ratio is decisive in controlling the deuteron loading flux in palladium – and thus LANR. Successful LANR experiments reflect the 'war' between applied electrical energy which is organizing the deuterons versus their randomization by thermal disorganization.

The second term includes the first-order deuteron loss rates by gas evolution and the desired fusion process(es). The minus sign means that the second term heralds that competitive gas evolving reactions at the metal electrode surface can destroy (quench) the desired reactions. The first-order loading flux rate constant ( $k_E$ ) is dependent upon the applied electric field intensity minus the first-order gas loss rate constant resulting from gas ( $D_2$ ) evolution at the cathode ( $k_G$ ). This implication is exactly opposite conventional "wisdom" that LANR is 'fusion by electrolysis' [1–4]. LANR can be missed by insufficient loading, contamination (effecting  $k_E$ , by protons or salt), and by the evolution of  $D_2$  gas, which all inhibit ("quench") the desired LANR reactions [3,4]. Note that Eq. (3) with the Einstein relation is similar to some flux equations from solid state physics, so there is the question of similarity of deuterons and their holes in Pd to holes and electrons in semiconductor materials.

## 5. Interpretation – Impact on Loading Rate

We believe the applied magnetic field intensity directly changes the loading rate of deuterons in to a metal deuteride. The following explains the reasons, and derives the equations demonstrating the relationship. Consider the role of

cathodic photo-irradiation in LANR. In addition to entry into the skin depth layer of the metal, a part of the impact is due to reflection off the cathode back into the double layer. Deuteron injection into the palladium increases (activation energy of  $\sim 14$  kcal per mol) from microwave rotation and IR vibration for the intermolecular transfer of deuterons to the Pd [33]. Hagelstein, Letts and Cravens [11,12] have also reported both single and dual photon impacts on cathodes as increasing excess heat. As we reported, there is a small and reproducible photo-incremental increase in both the power gain and in the observed excess heat from the coherent irradiation of the cathode, even when heating effects of the beam were included in the calibration. Near the OOP, the optical irradiation increased the excess power from  $84.7 \pm 10$  to  $95.5 \pm 12$  mW. For  $\sim 250$  mW input electrical power, the irradiation increased the excess power from  $79.8 \pm 7.6$  to  $93.3 \pm 6.3$  mW. Beyond the OOP, the impact of coherent non-ionizing radiation upon the cathode is small compared to dark heat production (power gain  $1.49 \pm 0.005$  in the dark,  $1.50 \pm 0.005$  for the laser irradiation, for input power levels which produce 400 mW excess heat). Incremental photoinduced excess power was observed only in the presence of a functioning active loaded cathode. This photoinduced excess power may be a lower limit. Issues of good optical path geometry, angle of penetration, active irradiated cathodic area, possible double layer interactions, interference with low dielectric constant bubbles formed and skin depth penetration remain relevant and suggest that the actual impact of laser irradiation may be greater.

We discovered that the effects are partially extra-cathodic. Therein lies the “rub”. Even though there is an incremental photo-thermoelectric increase in excess heat production changing the net excess power from 1.7 to  $1.8 \pm 0.1$  W, with optical irradiation of the cathode and surrounding solution, there is an additional change. Irradiation of the cathode necessarily results in irradiation of the solution and a photoinduced decrease in the Pt/D<sub>2</sub>O/Pd electrical resistance which increased the input electrical power dissipated (not excess). Optical irradiation of the cathodic volume and surrounding solution produces a photoinduced decrease in the effective cell-solution electrical resistance (55–51 kΩ). This increases the input electrical power for the same applied voltage. Because of the relationship between power gain (non-dimensional), excess power and input electrical power (watts), there follows a photoinduced decrease of the power gain, which is noticeable at higher input electrical power levels (2.4–2.3, for 1.3 W input).

This paradoxical decrease in the power gain heralds conduction/polarization pathways which lead away from some desired reactions. Exactly why this occurs can be understood by analysis of the modified loading flux equation. Examination of the LANR loading rate equations reveals that there are at least two ways the applied magnetic field can interact in the solution, through the ordering energy ratio and diffusivity of deuterons at the surface (first term), and through the solution resistance (second term).

Assuming a Faradaic efficiency for gas formation of  $\xi_g$  per electron, an electric current  $I$ , and accounting for the Faraday ratio to the mole,  $F$ , then

$$K_g \approx \frac{\xi_g I}{FA[D^+]}. \quad (4)$$

Substituting the electrical admittance with electrical conductivity with geometric factors, yields

$$K_g \approx \frac{\xi_g \sigma_{D_2O} V}{FL[D^+]}. \quad (5)$$

As a result, the modified LANR loading rate equation becomes

$$k_e \cong \frac{B_D q V}{L k_B T} - \frac{\xi_g \sigma_C V}{FL[D^+]}. \quad (6)$$

The term  $\sigma_C/L$  can be replaced by  $1/AR$  ( $A$  is the area,  $R$  is the solution electrical resistance (ohms)).  $R$  is in the denominator of the second term. This is a very important equation because, first, the first-order loading rate decreases (“is quenched”) with increasing solution electrical conductivity (or decreasing electrical resistance). This equation predicts the response of LANR to an applied magnetic field intensity in an LANR system. If the applied magnetic field

intensity is sufficient, this term may dominate, actually increasing the system performance. Increasing the solution electrical resistance ( $R$ ) increases LANR loading. The converse, through the second term can end all loading and LANR performance.

Second, in addition, the changes in vectors from the applied magnetic field intensity, with the observed decreased electrophoretic mobility, may be the etiology of some of the morphologies reported by Szpak, Gordon and Mosier-Boss [47,19,41].

## 6. Conclusion – Possibility of Increased Loading

An applied magnetic field ( $\sim 0.3$  T) to the high impedance DAP (Dual anode PHUSOR(R) type) LANR system increases the LANR solution's electrical resistance  $\sim 10$ – $17\%$ . The time constant for change was on the order of minutes. The incremental resistance increase to an applied H-field is greatest at low input loading and driving electrical currents. The incremental resistance increase to an applied H-field is greatest with the applied H-field perpendicular to the applied driving electrical field (E-field) intensity.

The modified LANR loading rate equation indicates that an applied H-field may increase loading in a LANR system by increasing solution resistance. Our past studies, which examined the impact of laser irradiation on LANR cathodes has taught us that any change of solution electrical resistance will directly impact LANR performances through the modified deuteron loading rate equation.

In this paper, it is shown that if an applied magnetic field intensity is sufficient, especially perpendicular to the applied electric field intensity and at lower electrical driving currents, an increase in system performance is expected from increased loading, resulting from an increase in solution electrical resistance. In the future, we anticipate reporting and discussing the observed and expected findings in LANR systems, with various arrangements of applied magnetic field intensities.

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